

# **Numerical Homogenization of Viscoelastic Composites with Piezoelectric Fibers**

**Mohammed Al-Ajmi, Ph.D.**

**Associate Professor**

**Prabha Muthusamy, Ph.D.**

**Research Assistant**

**Mechanical Engineering Department Kuwait University**



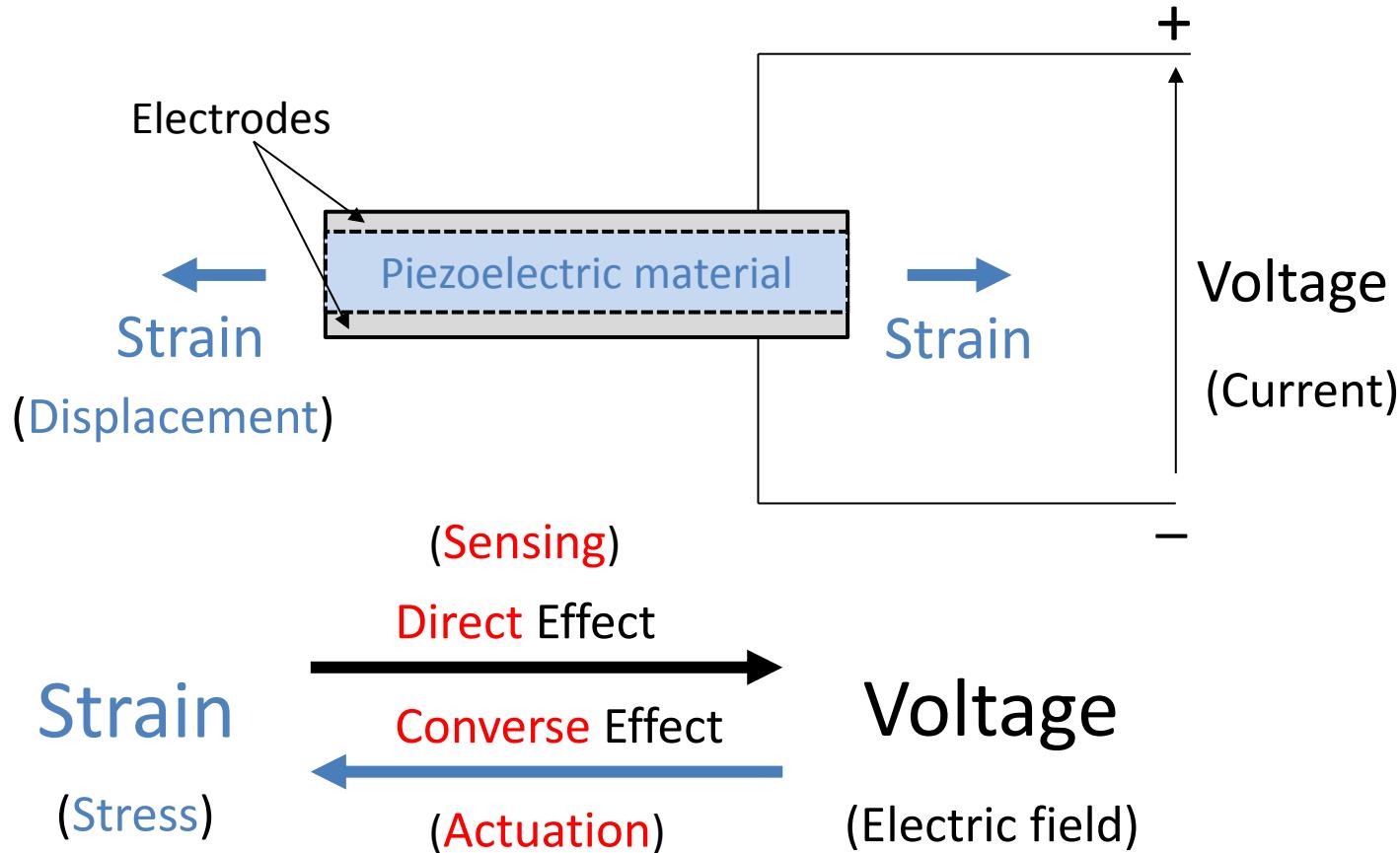
# Layout

- Introduction
- Theoretical Formulation
- Numerical Analysis
- Conclusion



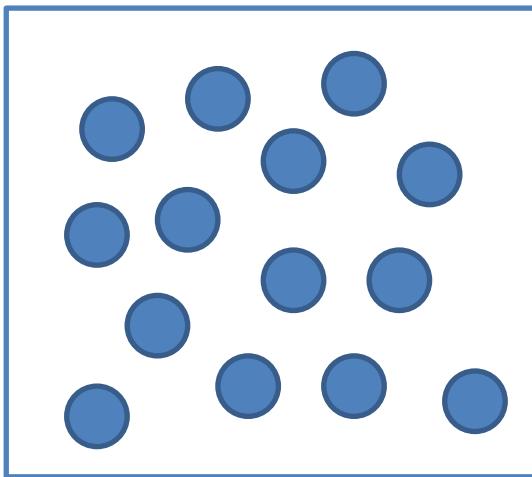
# Introduction

## Piezoelectric effects:

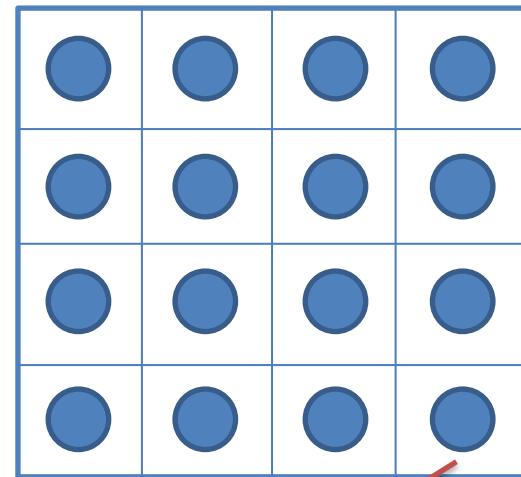


# Introduction

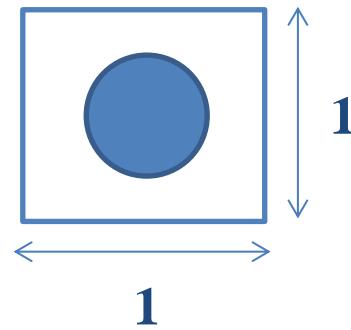
Real



Assumed

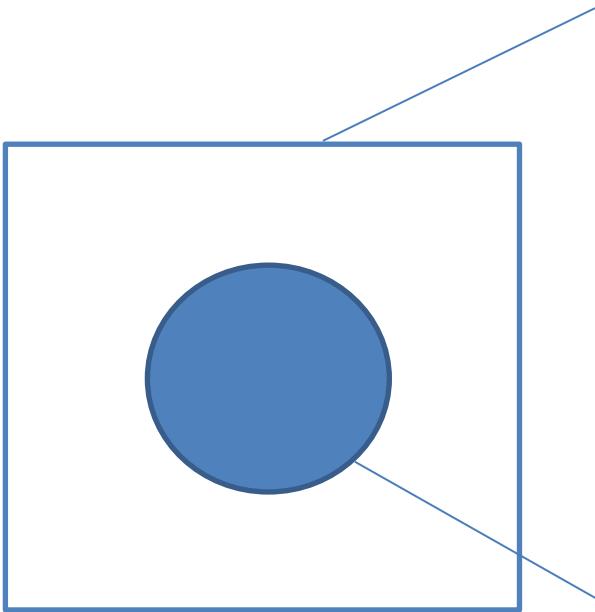


Representative Unit Cell



# Introduction

Piezo-Visco  
Composite



- Matrix**
  - Square
  - Linear Visco-elastic
  
- Fiber**
  - Circular
  - Linear Piezo-electric
  - Poled in Fiber direction

# Theoretical Formulation

## Linear Piezoelectric Constitutive Equations:

e-form (used in FEA):

$$\mathbf{T} = \mathbf{C}^E \mathbf{S} - \mathbf{e}^t \mathbf{E}$$

$$\mathbf{D} = \mathbf{e} \mathbf{S} + \epsilon^s \mathbf{E}$$



# Theoretical Formulation

## Linear Piezoelectric Constitutive Equations:

$$\begin{aligned} \mathbf{T} &= \mathbf{C}^E \mathbf{S} - \mathbf{e}^t \mathbf{E} \\ \mathbf{D} &= \mathbf{e} \mathbf{S} + \epsilon^s \mathbf{E} \end{aligned}$$

Stress                                  Strain  
At constant Electric Field

Electric Field

Electrical Displacement              Permittivity  
At constant strain

Elastic Coefficients  
At constant Electric Field

Stress Piezoelectric  
Coupling Coefficients



# Theoretical Formulation

## Linear Isotropic Viscoelastic Material:

$$E(w) = E(\zeta w) + iE(\zeta w)$$

$$h = \frac{E(\zeta w)}{E(\zeta w)} \quad \longrightarrow \quad E(w) = E(\zeta w)(1 + ih)$$



# Theoretical Formulation

## Homogenization:

$$\bar{T}_{ij} = \frac{1}{V} \underset{V}{\oint} T_{ij} dV$$

$$\bar{D}_{ij} = \frac{1}{V} \underset{V}{\oint} D_{ij} dV$$

$$\bar{S}_{ij} = \frac{1}{V} \underset{V}{\oint} S_{ij} dV$$

$$\bar{E}_{ij} = \frac{1}{V} \underset{V}{\oint} E_{ij} dV$$

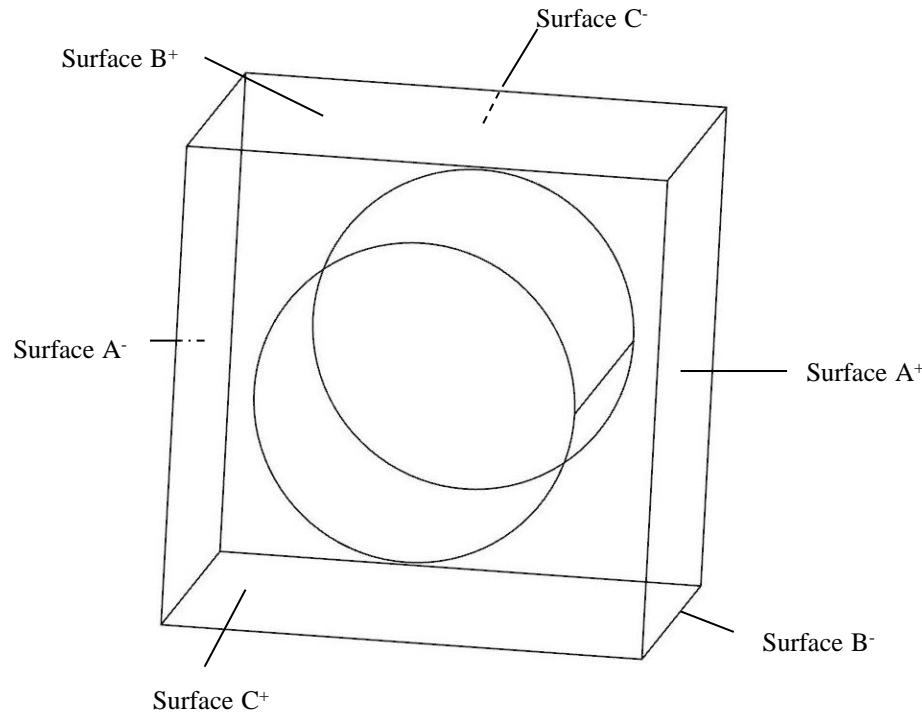
$$\bar{T} = \hat{C}(w) \bar{S} - \hat{e}(w)^T \bar{E}$$

$$\bar{D} = \hat{e}(w) \bar{S} + \hat{e}(w) \bar{E}$$



# Numerical Analysis

Geometry of representative volume element:



# Numerical Analysis

- Viscoelastic material is modeled using:

$$M_0(s) = D_0 + \frac{D_1 n!}{s^n}$$

$D_0$  is the initial elastic compliance,  
 $D_1$  and  $n$  are experimentally determined parameters, and  
 $s=i\omega$ . with  $\omega$  denoting the frequency.

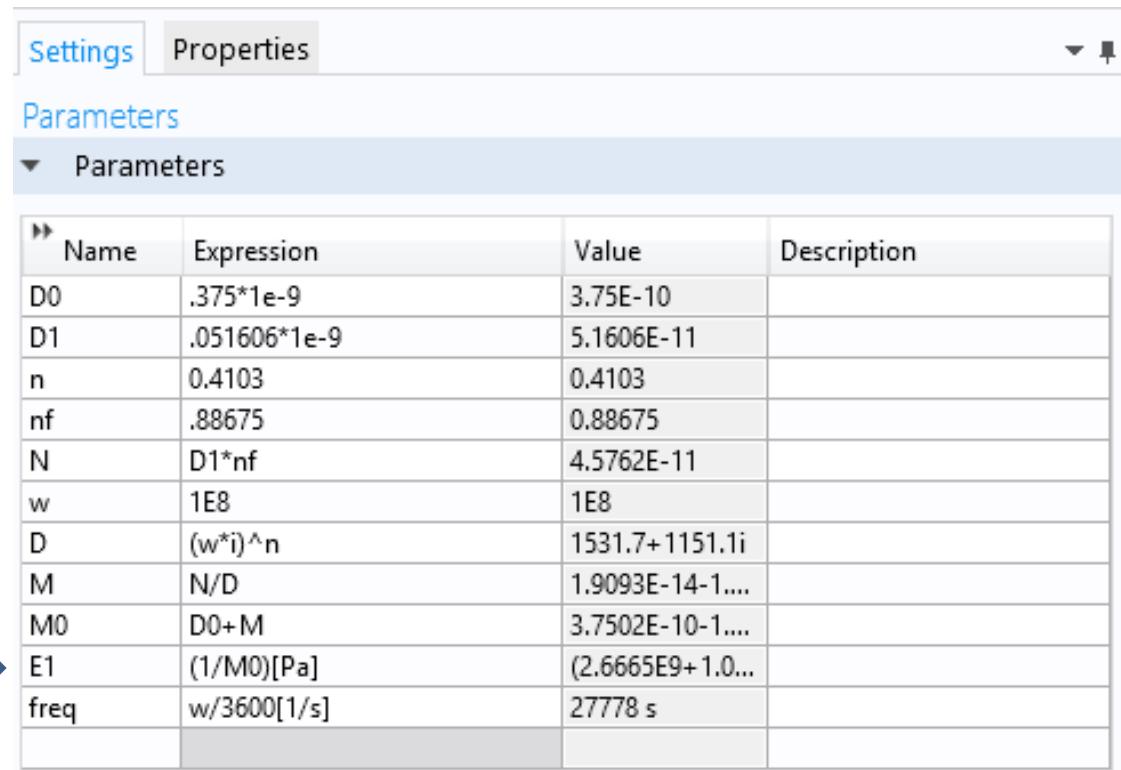
The Young modulus  $E$  is taken as the inverse of  $M_0(s)$

- Piezoelectric Material used: PZT-7A



# Numerical Analysis

Frequency-dependent viscoelastic material implementation in COMSOL



The screenshot shows the 'Parameters' section of the COMSOL interface. The 'Properties' tab is selected. A table lists the following parameters:

Name	Expression	Value	Description
D0	.375*1e-9	3.75E-10	
D1	.051606*1e-9	5.1606E-11	
n	0.4103	0.4103	
nf	.88675	0.88675	
N	D1*nf	4.5762E-11	
w	1E8	1E8	
D	(w*i)^n	1531.7+1151.1i	
M	N/D	1.9093E-14-1....	
M0	D0+M	3.7502E-10-1....	
E1	(1/M0)[Pa]	(2.6665E9+1.0...	
freq	w/3600[1/s]	27778 s	

Youngs modulus in terms of frequency



# Numerical Analysis

Settings Properties

Material

Label: Material 2

Geometric Entity Selection

Geometric entity level: Domain

Selection: Manual

Active

Override

Material Properties

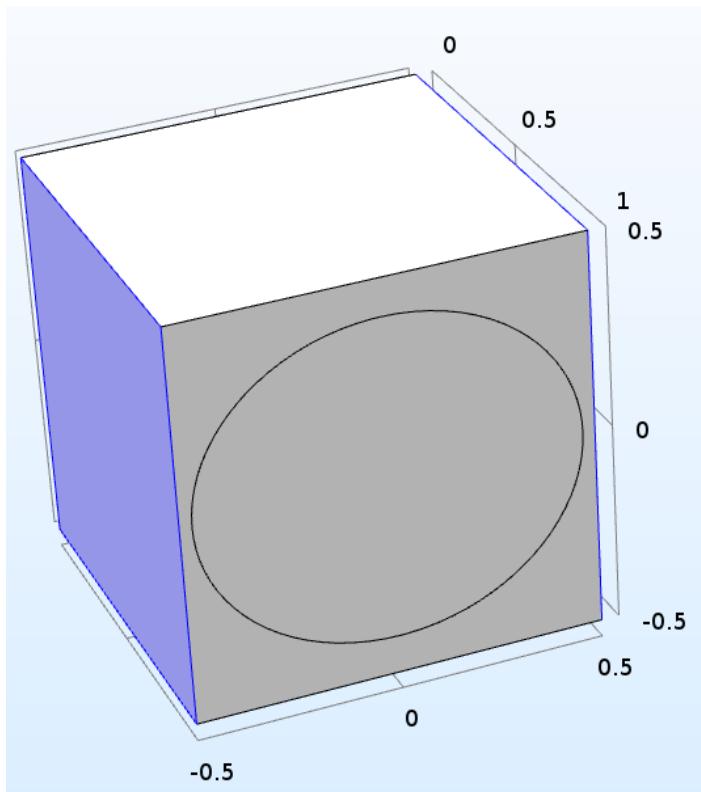
Material Contents

Property	Name	Value	Unit	Property group
Density	rho	1370	kg/m <sup>3</sup>	Basic
Relative permittivity	epsilon_r	2.8	1	Basic
Young's modulus	E	E1	Pa	Young's modulus an
Poisson's ratio	nu	0.367	1	Young's modulus an



# Numerical Analysis

## Periodicity Condition



Settings  
Periodic Condition

Label: Periodic Condition 3

### Boundary Selection

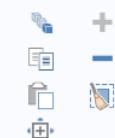
Selection: Manual



1

12

Active



### Override and Contribution

### Equation

Show equation assuming:

Study 1, Stationary

### Periodicity Settings

Type of periodicity:

User defined

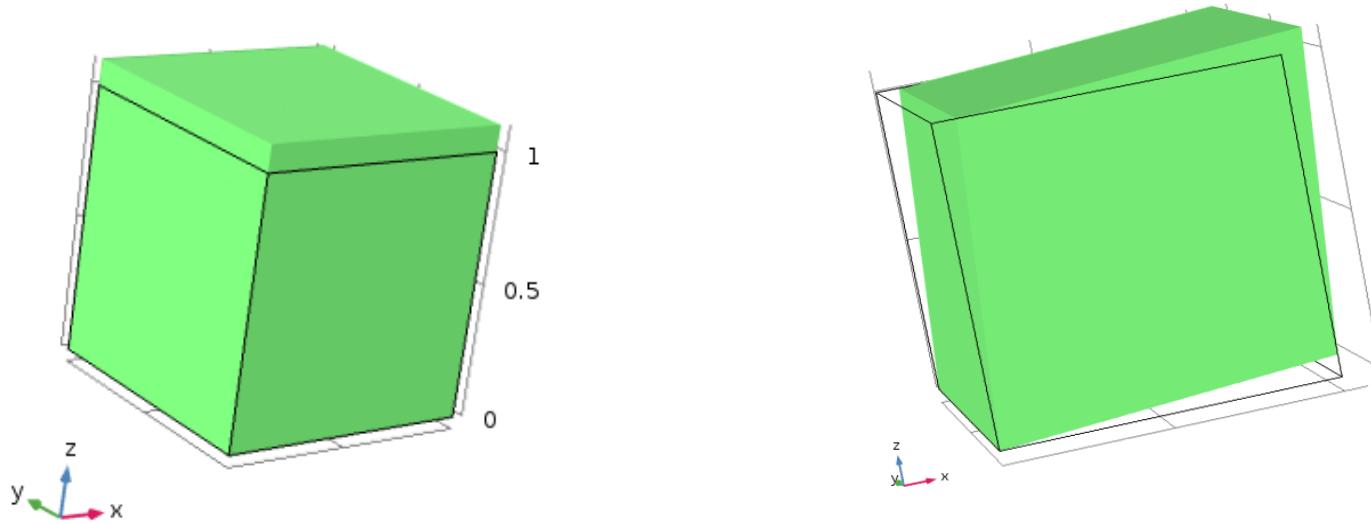
Periodic in u

Periodic in v

Periodic in w

# Numerical Analysis

Deformed Viscoelastic material under normal and shear load

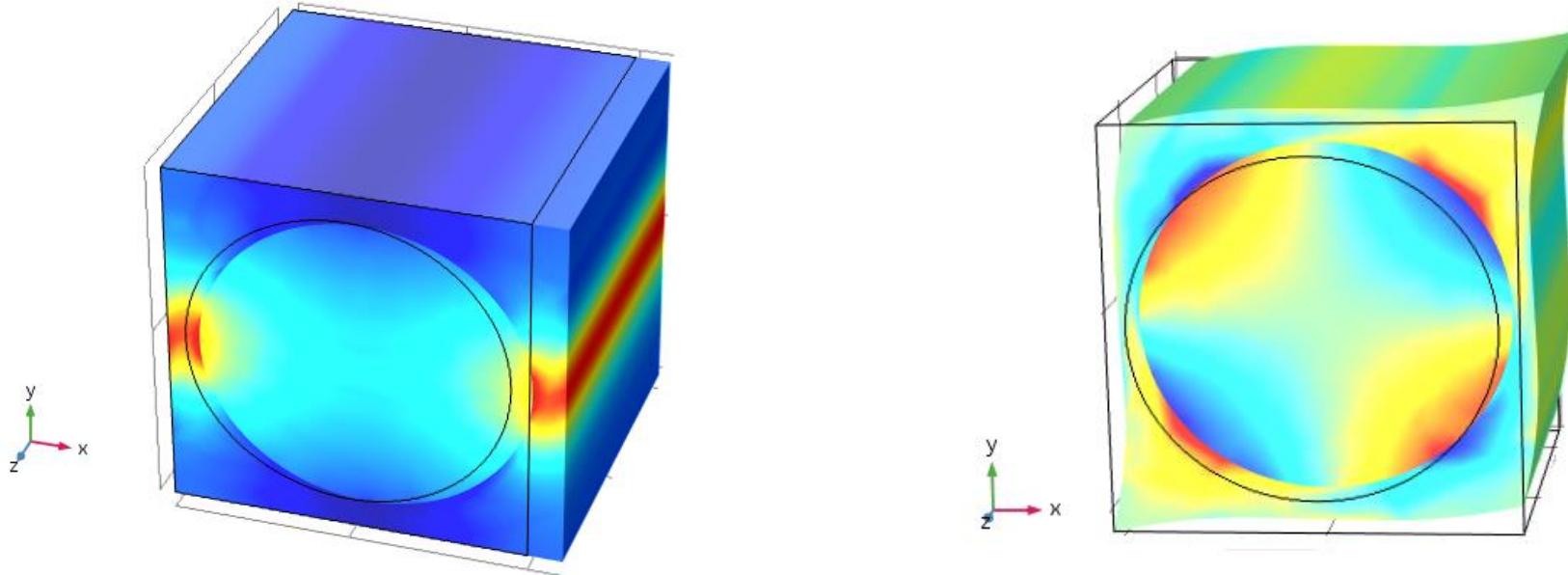


**Figure 3:** Deformed unit cell of viscoelastic material

# Numerical Analysis

## Sample Mechanical Calculation:

-Apply normal and shear on the cell cross section (all potentials =0)



$$C_{11} = \frac{\bar{T}_{11}}{\bar{S}_{11}}$$

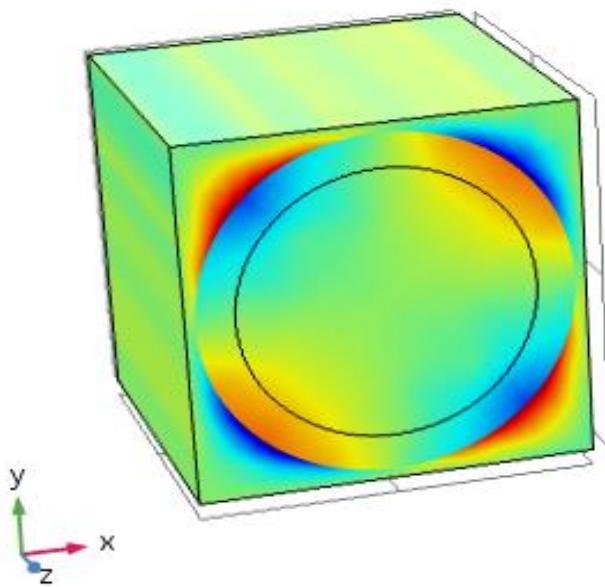
$$C_{66} = -\frac{\bar{T}_{11}}{\bar{S}_{12}}$$

Figure 4: Deformed unit cell of viscoelastic matrix reinforced with PZT fiber

# Numerical Analysis

## Sample Piezoelectric Calculation

-Apply potential difference across fiber (all displacements =0)

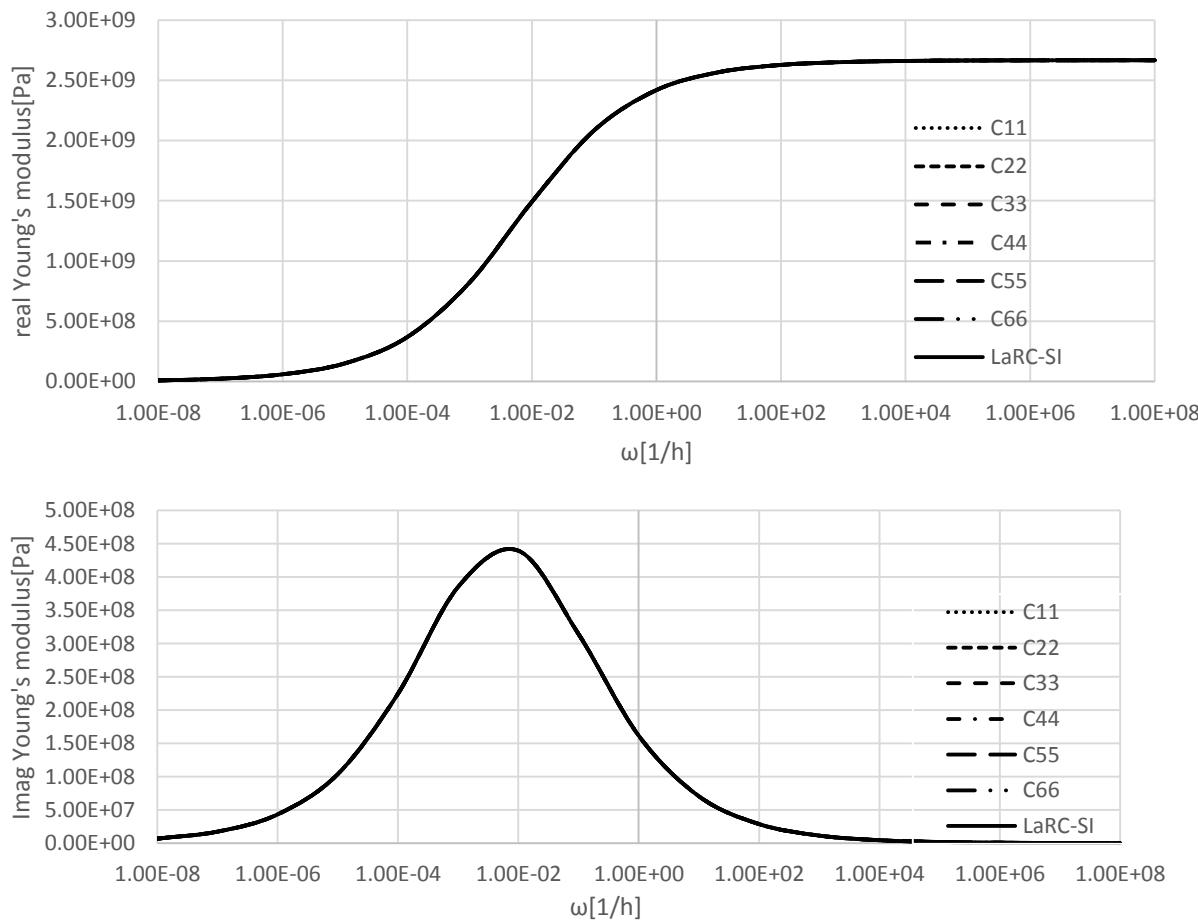


$$\hat{e}_{31} = \frac{\overline{T}_{11}}{\overline{E}_3}$$

**Figure 4:** Deformed unit cell of viscoelastic matrix reinforced with PZT fiber



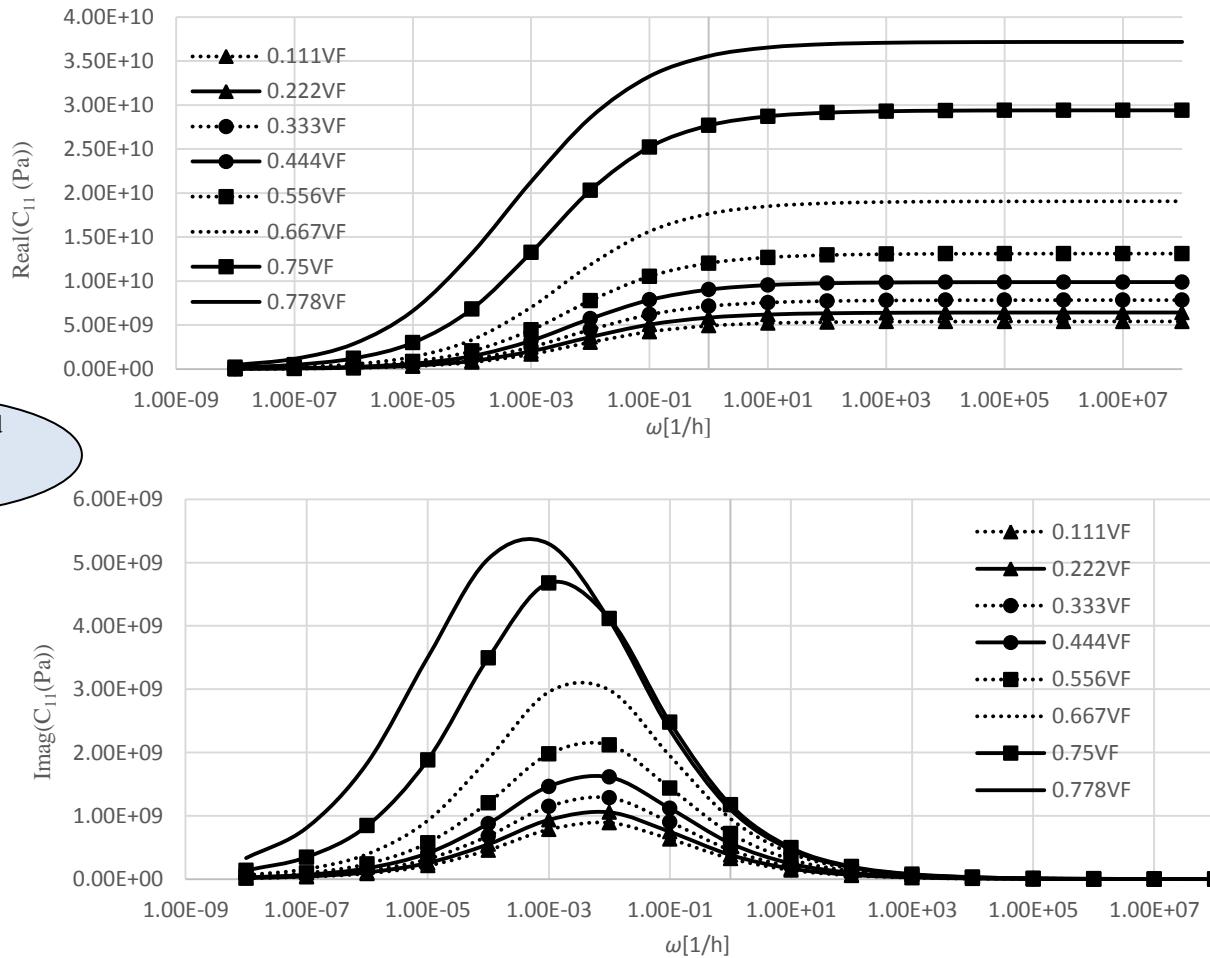
# Results



**Figure 5.** Real and Loss Modulus LaRC-SI with respect to frequency for different boundary condition.

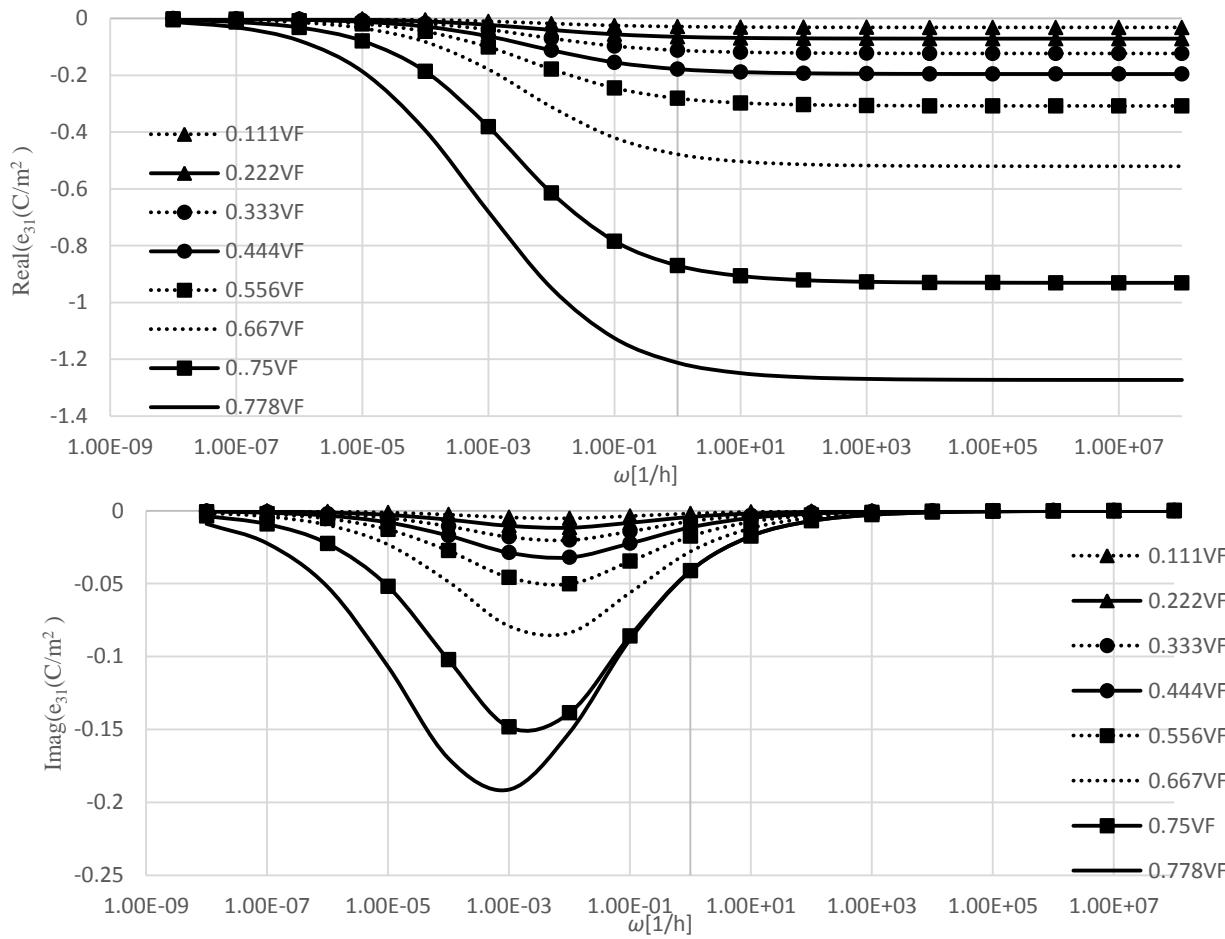


# Results



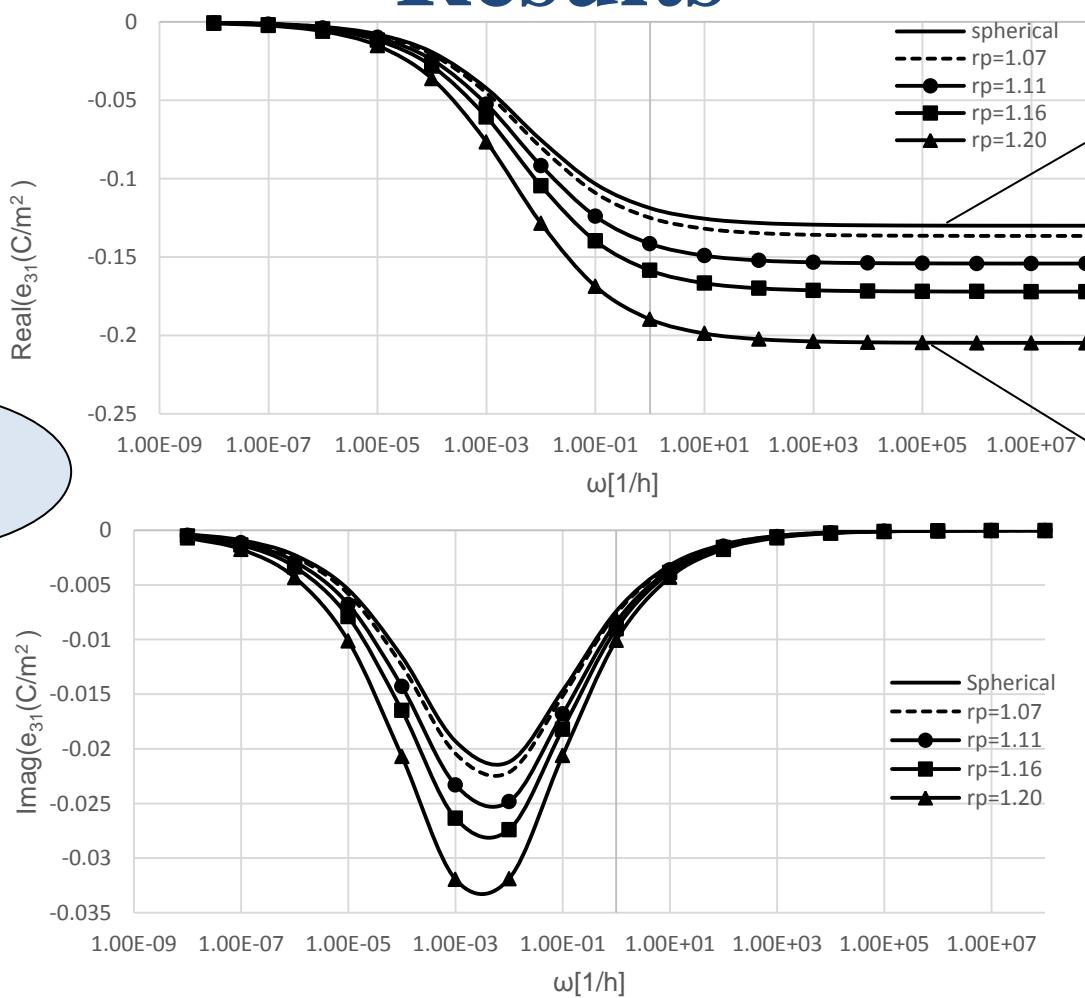
**Figure 6 .** Effective storage and loss elastic modulus ( $C_{11}$ ) for a viscoelectroelastic composite for different volume fraction.

# Results

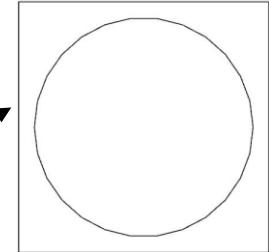


**Figure 7.** Effective storage and loss piezoelectric modulus ( $e_{31}$ ) for a viscoelectroelastic composite for different volume fraction.

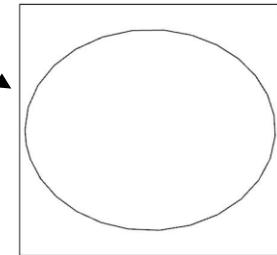
# Results



PZT fiber reinforced  
in viscoelastic matrix  
with different fiber  
cross section.



**spherical fiber  
unit cell**



**ellipsoidal fiber  
unit cell**

**Figure .** Effective storage and loss piezoelectric modulus ( $e_{31}$ ) for a viscoelectroelastic composite.

**Major to minor axis ratio of the ellipse is  $rp$ .**



# Conclusions

- The results shows that the material properties strongly depend on:
  - Frequency-dependent viscoelastic properties
  - Piezoelectric fiber volume fraction
- COMSOL directly calculates the frequency-dependent properties with no need for customized functions/subroutines for material properties or periodic BCs

